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Amplifiers and active antennas for TV broadcast reception in domestic premises; Harmonised standard for access to radio spectrum

Reference

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Keywords

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Foreword

This draft Harmonised European Standard (EN) has been produced by ETSI Technical Committee Electromagnetic compatibility and Radio spectrum Matters (ERM), and is now submitted for the combined Public Enquiry and Vote phase of the ETSI Standardisation Request deliverable Approval Procedure.

The present document has been prepared under the Commission's standardisation request C(2015) 5376 final [i.4] to provide one voluntary means of conforming to the essential requirements of Directive 2014/53/EU on the harmonisation of the laws of the Member States relating to the making available on the market of radio equipment and repealing Directive 1999/5/EC [i.1].

Once the present document is cited in the Official Journal of the European Union under that Directive, compliance with the normative clauses of the present document given in Table A.1 confers, within the limits of the scope of the present document, a presumption of conformity with the corresponding essential requirements of that Directive and associated EFTA regulations.

Other Union legislation may be applicable to the product(s) falling within the scope of the present document.

Proposed national transposition dates	
Date of latest announcement of this EN (doa):	3 months after ETSI publication
Date of latest publication of new National Standard or endorsement of this EN (dop/e):	6 months after doa
Date of withdrawal of any conflicting National Standard (dow):	18 months after doa

Modal verbs terminology

In the present document "**shall**", "**shall not**", "**should**", "**should not**", "**may**", "**need not**", "**will**", "**will not**", "**can**" and "**cannot**" are to be interpreted as described in clause 3.2 of the ETSI Drafting Rules (Verbal forms for the expression of provisions).

"**must**" and "**must not**" are **NOT** allowed in ETSI deliverables except when used in direct citation.

Introduction

The present document is a Harmonised Standard for amplifiers and active antennas used for broadcast TV reception in the UHF band from 470 MHz to 694 MHz and the VHF band from 174 MHz to 230 MHz.

The primary purpose of the present document is to specify technical parameters to limit the interfering effects caused by unwanted signals on TV reception.

1 Scope

The present document specifies technical characteristics and methods of measurements for:

1) Indoor and outdoor amplifiers for broadcast TV and sound reception at UHF (470 MHz to 694 MHz) and at VHF (174 MHz to 230 MHz).

2) Indoor active antennas for broadcast TV and sound reception at UHF (470 MHz to 694 MHz) and at VHF (174 MHz to 230 MHz).

NOTE: The relationship between the present document and essential requirements of article 3.2 of Directive 2014/53/EU is given in annex A.

2 References

2.1 Normative references

References are either specific (identified by date of publication and/or edition number or version number) or non-specific. For specific references, only the cited version applies. For non-specific references, the latest version of the referenced document (including any amendments) applies.

Referenced documents which are not found to be publicly available in the expected location might be found at https://docbox.etsi.org/Reference.

NOTE: While any hyperlinks included in this clause were valid at the time of publication, ETSI cannot guarantee their long term validity.

The following referenced documents are necessary for the application of the present document.

[1] Void.

2.2 Informative references

References are either specific (identified by date of publication and/or edition number or version number) or non-specific. For specific references, only the cited version applies. For non-specific references, the latest version of the referenced document (including any amendments) applies.

NOTE: While any hyperlinks included in this clause were valid at the time of publication, ETSI cannot guarantee their long term validity.

The following referenced documents are not necessary for the application of the present document but they assist the user with regard to a particular subject area.

[i.1] Directive 2014/53/EU of the European Parliament and of the Council of 16 April 2014 on the harmonisation of the laws of the Member States relating to the making available on the market of radio equipment and repealing Directive 1999/5/EC.

[i.2] Void.

[i.3] Void.

[i.4] Commission Implementing Decision C(2015) 5376 final of 4.8.2015 on a standardisation request to the European Committee for Electrotechnical Standardisation and to the European Telecommunications Standards Institute as regards radio equipment in support of Directive 2014/53/EU of the European Parliament and of the Council.

[i.5] Void.

[i.6] ETSI TR 100 028 all parts (V1.4.1) (2001): "Electromagnetic compatibility and Radio spectrum Matters (ERM); Uncertainties in the measurement of mobile radio equipment characteristics".

[i.7] Void.

[i.8] Void.

3 Definitions of terms, symbols and abbreviations

3.1 Terms

For the purposes of the present document, the following terms apply:

active antenna: antenna equipped with an integrated low noise amplifier for indoor use (equipment type A)

amplifier: indoor or outdoor equipment intended to amplify terrestrial broadcast signals

category: method of classifying equipment according to its type {P,D,L} and selectivity class {1,2}

domestic amplifier: general purpose amplifier for use in domestic premises intended to amplify terrestrial broadcast signals (equipment type D)

internal immunity: ability of a device, equipment or system to perform without degradation in the presence of electromagnetic disturbances appearing at its normal input terminals or antennas

launch amplifier: high output level amplifier used to distribute terrestrial broadcast signals to multiple receivers (equipment type L)

preamplifier: low noise amplifier with one or more outputs typically used immediately after a terrestrial receive antenna (equipment type P)

NOTE: A masthead amplifier is a preamplifier for outdoor use with terrestrial broadcast signals.

UHF band: broadcast band from 470 MHz to 694 MHz divided into 28 channels, each 8 MHz wide, numbered from 21 to 48

VHF band: broadcast band from 174 MHz to 230 MHz divided into 8 channels, each 7 MHz wide, numbered from 5 to 12

3.2 Symbols

For the purposes of the present document, the following symbols apply:

nf	Noise Figure, expressed in dB
IM3	3rd order intercept

3.3 Abbreviations

For the purposes of the present document, the following abbreviations apply:

AAUT	Active Antenna Under Test
AC	Alternating Current
AUT	Amplifier Under Test
CW	Carrier Wave
DC	Direct Current
ENR	Excess Noise Ratio
E-UTRA	Evolved Universal Terrestrial Radio Access
F	Frequency
GTEM	Gigahertz Transverse ElectroMagnetic
IMD	InterModulation Distortion
IMT	International Mobile Telecommunication
MATV	Master Antenna TeleVision
RF	Radio Frequency

RL	Return Loss
SNR	Signal to Noise Ratio
TOI	Third Order Intercept
TV	TeleVision
UHF	Ultra High Frequency
VHF	Very High Frequency

4 Technical requirements specifications

4.1 Environmental profile

The technical requirements of the present document apply under the environmental profile for operation of the equipment, which shall be in accordance with its intended use. The equipment shall comply with all the technical requirements of the present document which are identified as applicable in annex A at all times when operating within the boundary limits of the operational environmental profile defined by its intended use.

4.2 General conditions of measurement

4.2.1 General

This clause gives the general operational conditions. The product-specific operating conditions will be derived from the product description and documentation and stated in the test report.

The levels of the test signals shall be expressed either in terms of the power relative to 1 mW (dBm) for amplifiers or the field strength relative to 1 µV/m (dBµV/m) for antennas.

4.2.2 Equipment configuration

Power and signal distribution, grounding, interconnecting cabling and physical placement of equipment of a test system shall simulate the typical application and usage in so far as is practicable, and shall be in accordance with the relevant product specifications.

4.2.3 Test conditions

4.2.3.1 General

The equipment shall be tested under normal test conditions according to the relevant product and basic standards including the information accompanying the equipment, and shall be within the range of humidity, temperature and supply voltage for the intended use. The test conditions shall be recorded in the test report.

The test configuration and mode of operation shall be representative of the intended use and shall be recorded in the test report.

Typical test equipment has a characteristic impedance of 50 Ω whilst antennas and amplifiers typically have a characteristic impedance of 75 Ω. Impedance matching shall be used to interface to the equipment under test.

The equipment under test shall be fed by the power adaptor supplied by the manufacturer or, for products supplied without a power adaptor, by a suitable equivalent.

For amplifiers with multiple inputs or multiple outputs, any ports that would otherwise be unconnected shall be terminated in a well-matched load. For devices with multiple inputs and outputs, all inputs and outputs shall be tested.

4.2.3.2 Normal test conditions

The normal temperature and humidity conditions for tests shall be a combination of temperature and humidity within the following ranges:

- temperature: +15 °C to +35 °C;
- relative humidity: 20 % to 95 %, non-condensing.

4.3 General assessment

The manufacturer shall at the time of submission of the equipment for test, supply the following information to be recorded in the test report:

- the intended functions of the equipment which shall be in accordance with the documentation accompanying the equipment;
- the equipment category, as defined in clause 4.4;
- the ancillary equipment (power supply for example) to be supplied with the equipment for testing (where applicable);
- an exhaustive list of ports, classified as either power or signal. Power ports shall further be classified as AC or DC power;
- the operating frequency ranges over which the equipment is intended to operate;
- the environment(s) in which the equipment is intended to be used.

4.4 Equipment categorization

The equipment covered by the present document is classified according to Tables 1 and 2. The equipment type and selectivity classification appropriate for the RF environment are combined to describe an equipment category.

Table 1: Equipment types

Equipment Type	Description	Notes
P	Preamplifiers	Low noise amplifiers with one or more outputs.
D	Domestic amplifiers	Amplifiers with one or more outputs not intended for low noise applications.
L	Launch amplifiers	High output level amplifiers used for MATV systems.
A	Active antennas	Amplified domestic antenna for indoor use.

Table 2: RF environment and selectivity classification

Selectivity Classification	Intended RF environment	Notes
1	IMT is deployed above 700 MHz (E-UTRA band 28 and band 20). Devices have selectivity to reject IMT signals above 700 MHz.	Provides selectivity to reject LTE-700 (E-UTRA band 28) and LTE-800 (E-UTRA band 20) signals.
2	IMT is deployed above 700 MHz and/or below 470 MHz. Devices have selectivity to reject IMT signals below 470 MHz and above 700 MHz.	Provides selectivity to reject LTE-700 (E-UTRA band 28), LTE-800 (E-UTRA band 20) and IMT signals below 470 MHz.

For example, equipment type P and selectivity classification 1 denotes a wideband preamplifier (equipment category P1) intended for use where IMT is deployed in the range from 694 MHz to 862 MHz.

4.5 Conformance requirements

4.5.1 Void

Table 3: Void

4.5.2 Noise figure

4.5.2.1 Definition

The noise figure, *nf*, is defined as the degradation of the Signal-to-Noise Ratio (SNR) resulting from noise generated by the amplifier expressed in decibel notation:

$$nf = 10 \times log_{10} \frac{C_1/N_1}{C_2/N_2}$$

where: C_1= power of input signal;

C_2 = power of output signal;

N_1 = power of noise at input (thermal noise at 290 K);

N_2 = power of noise at output (thermal noise at 290 K).

The noise figure (*nf*) is defined at the standard noise temperature (290 K) over the bandwidth of interest.

4.5.2.2 Limits

The maximum noise figure shall be less than or equal to the values specified in Table 4.

Table 4: Amplifier noise figure

Test number	Test description	Test Frequencies (MHz)	Maximum noise figure (dB)		
				Category {P,D}{1,2}	Category {L}{1,2}
1	Noise figure UHF amplifiers	F_0		4	7
		F_1			
		F_2			
2	Noise figure VHF amplifiers	205,5		4	7
NOTE: The test frequencies F_0, F_1, F_2 are defined in Table 5.					

Table 5: Test frequencies

Test Frequencies (MHz)		Category {P,D,L}{1}	Category {P,D,L}{2}		
F_0		470	478		
F_1		586	586		
F_2		686	686		
NOTE: For amplifiers operating over a reduced frequency band, the test frequencies shall be as follows: F_0 = minimum frequency + 8 MHz, F_1 = centre frequency and F_2 = maximum frequency - 8 MHz of the stated band of operation.					

4.5.2.3 Conformance

The conformance tests for this requirement shall be as described in clause 5.3.2.

4.5.3 Amplifier intermodulation

4.5.3.1 Definition

Intermodulation distortion is a non-linear distortion characterized by the appearance of output signals at frequencies corresponding to the sum and difference of the fundamentals and harmonics of the signals applied at the input. The linearity of an RF amplifier is characterized in terms of its Third Order Intercept (TOI), which is measured using a two-tone test. Wanted signals at frequencies F_1 and F_2 are applied at the amplifier input and the non-linearity manifests itself in the form of unwanted third order intermodulation products at the output generated at frequencies $2 \times F_1 - F_2$ and $2 \times F_2 - F_1$.

The third-order input intercept (TOI_{input}) value is an imaginary point corresponding to the input level of each of a pair of CW tones that would generate equal levels of the wanted and unwanted third-order products at the output of the amplifier. This point is never reached, as an amplifier will saturate before this condition can occur, but it is useful as it allows the level of intermodulation distortion to be predicted at a given input signal level.

4.5.3.2 Limits

The value of TOI_{input} shall exceed the values shown in Table 6.

Table 6: Third order input intercept limits

Test number	Test description	Test Frequencies (MHz)	Minimum Input Intercept (dBm) Category {P,D,L}{1,2}
1	UHF amplifier input TOI	F_0	-4
		F_1	
		F_2	
2	VHF amplifier input TOI	205,5	-4
NOTE: The test frequencies F_0, F_1, F_2 are defined in Table 5.			

4.5.3.3 Conformance

The conformance tests for this requirement shall be as described in clause 5.3.3.

4.5.4 Return loss

4.5.4.1 Definition

The return loss, *RL*, is a measure of the attenuation of the reflected signal, P_{ref}, relative to the incident signal, P_{inc}, that results when an amplifier (or other RF component) is connected to an RF system of a given characteristic impedance Z_0. The reflected signal results from a mismatch between the characteristic impedance of the system and the terminal impedances of the amplifier.

$$RL(dB) = -10 \times log_{10}(\frac{P_{ref}}{P_{inc}})$$

$$= -20 \times log_{10}\left|\frac{(Z_a - Z_0)}{(Z_a + Z_0)}\right|$$

where:

Z_a is the impedance of the amplifier (defined separately at the input and output).

Z_0 is 75 Ω.

P_{ref} is the power reflected by the AUT in the linear domain.

P_{inc} is the incident power in the linear domain.

The return loss is thus a measure of mismatch between the amplifier (input or output) impedance and the characteristic impedance of the RF system.

4.5.4.2 Limits

The minimum input return loss at the input port (RL_{input}) shall be equal to or greater than the values in Table 7.

Table 7: Input return loss limits

Test number	Test description	Test Frequencies (MHz)	Minimum input return loss (dB)	
			Category {P}{1,2}	Category {D,L}{1,2}
1	UHF amplifier input return loss	F_0	5	8
		F_1		
		F_2		
2	VHF amplifier input return loss	205,5	5	8
NOTE: The test frequencies F_0, F_1, F_2 are defined in Table 5.				

The minimum output return loss at the output port (RL_{output}) shall be equal to or greater than the values in Table 8.

Table 8: Output return loss limits

Test number	Test description	Test Frequencies (MHz)	Minimum output return loss (dB)	
			Category {P}{1,2}	Category {D,L}{1,2}
1	UHF amplifier output return loss	F_0	8	8
		F_1		
		F_2		
2	VHF amplifier output return loss	205,5	8	8
NOTE: The test frequencies F_0, F_1, F_2 are defined in Table 5.				

4.5.4.3 Conformance

The conformance tests for this requirement shall be as described in clause 5.3.4.

4.5.5 Selectivity

4.5.5.1 Definition

The adjacent band selectivity is a measure of the resilience to IMT interference above and/or below the UHF broadcast band.

4.5.5.2 Limits

4.5.5.2.1 Classification 1

The relative gain shall not exceed the limits specified in Table 9, additionally shown in Figure 1.

Table 9: Adjacent band selectivity limits (classification 1)

Frequency (MHz)	Relative gain g_r (dB)	
	Maximum (dB)	Minimum (dB)
470 < F ≤ 686	+2	-2
686 < F ≤ 694	+2	-4
694 < F ≤ 703	+2	-
703 < F ≤ 738	-10	-
738 < F ≤ 960	-25	-

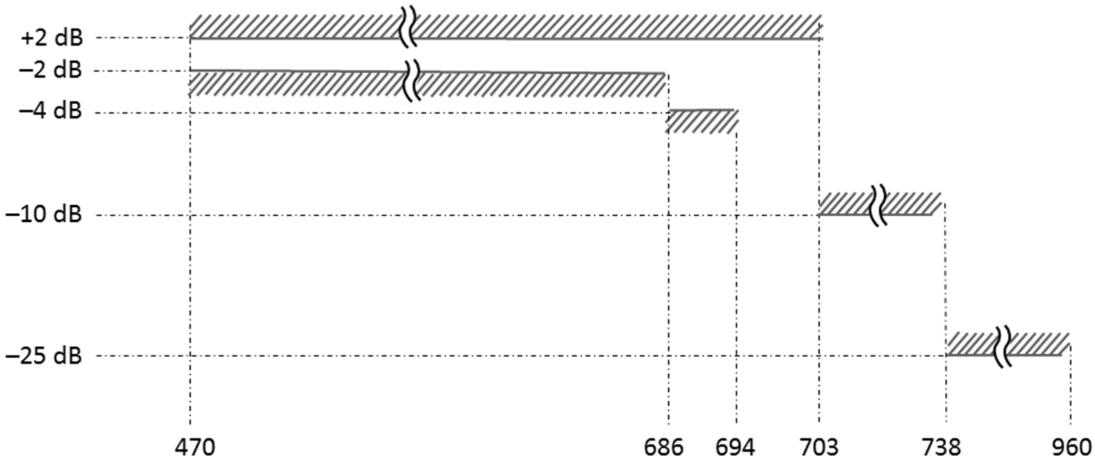


Figure 1: Adjacent band selectivity limits (classification 1)

4.5.5.2.2 Classification 2

The relative gain shall not exceed the limits specified in Table 10, additionally shown in Figure 2.

Table 10: Adjacent band selectivity limits (classification 2)

Frequency (MHz)	Relative gain g_r (dB)	
	Maximum (dB)	Minimum (dB)
410 < F ≤ 467	-10	-
467 < F ≤ 470	+2	-
470 < F ≤ 478	+2	-4
478 < F ≤ 686	+2	-2
686 < F ≤ 694	+2	-4
694 < F ≤ 703	+2	-
703 < F ≤ 738	-10	-
738 < F ≤ 960	-25	-

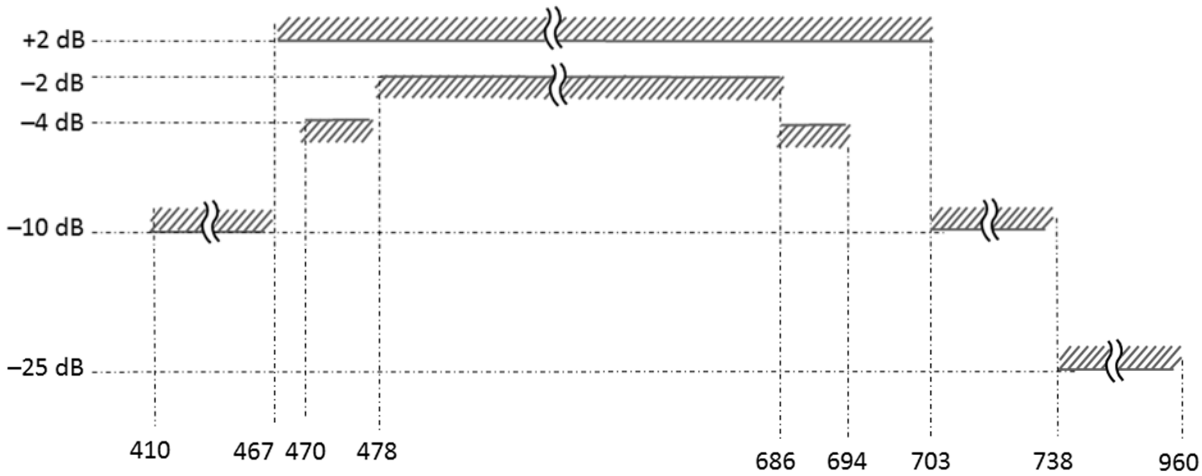


Figure 2: Adjacent band selectivity limits (classification 2)

4.5.5.3 Conformance

The conformance tests for this requirement shall be as described in clause 5.3.5.

4.5.5.4 Void

Table 11: Void

Figure 3: Void

4.5.5.5 Void

Table 12: Void

Figure 4: Void

4.5.5.6 Void

4.5.6 Active antenna gain

4.5.6.1 Definition

The active antenna gain is defined as the sum of the passive antenna gain and the amplifier gain.

4.5.6.2 Limits

The active antenna gain shall fall between the minimum and maximum values given in Table 13.

Table 13: Active antenna gain limits

Test number	Test description	Frequency test points			Category {A}{1,2}	
		Start (MHz)	Mid (MHz)	Stop (MHz)	Minimum gain (dBi)	Maximum gain (dBi)
1	UHF antenna gain	478	582	686	6	20
2	VHF antenna gain	181	202	223	3	17

NOTE 1: For antennas operating over a reduced frequency band, test frequencies corresponding to the minimum frequency + 8 MHz, centre frequency, and maximum frequency - 8 MHz of the stated band of operation shall be chosen.

NOTE 2: The maximum gain measured over the specified test frequencies shall be equal to or greater than the gain stated by the manufacturer.

4.5.6.3 Conformance

The conformance tests for this requirement shall be as described in clause 5.3.6.

4.5.7 Active antenna figure of merit

4.5.7.1 Definition

The Figure of Merit (FoM) for an active antenna is the passive antenna gain, g_i, less the amplifier noise figure f_a. For further technical details, see annex B.

4.5.7.2 Limits

The minimum *FoM* shall exceed the values in Table 14 at each of the specified test frequencies.

Table 14: Antenna figure of merit

Test number	Test description	Test Frequencies (MHz)	Category {A}{1,2} Minimum FoM , $(g_i - f_a)$ (dB)
1	UHF antenna FoM	478	-5
		582	
		686	
2	VHF antenna FoM	205,5	-8
NOTE: For antennas operating over a reduced frequency band, test frequencies shall be chosen as follows: minimum frequency + 8 MHz, centre frequency, maximum frequency - 8 MHz.			

4.5.7.3 Conformance

The conformance tests for this requirement shall be as described in clause 5.3.7.

4.5.8 Active antenna intermodulation

4.5.8.1 Definition

Intermodulation distortion is a non-linear distortion characterized by the appearance of frequencies corresponding to the sum and difference frequencies of the fundamentals and harmonics that are transmitted through the device.

The third-order input intercept (e_{toi}) value is an imaginary point corresponding to the input field strength of each of a pair of CW tones that would generate equal levels of the wanted and unwanted third-order products at the output of the active antenna. This point is never reached, as the active antenna will saturate before this condition can occur, but it is useful as it allows the level of intermodulation distortion to be predicted at a given input signal.

4.5.8.2 Limits

The minimum e_{toi} shall exceed the values in Table 15.

Table 15: Active antenna input intercept

Test number	Test description	Test Frequencies (MHz)	Category {A}{1,2 } Minimum e_{toi} (dBμV/m)
1	UHF antenna input intercept	478	130
		582	
		686	
2	VHF antenna input intercept	205,5	130
NOTE: For antennas operating over a reduced frequency band, test frequencies shall be chosen as follows: minimum frequency + 8 MHz, centre frequency, maximum frequency - 8 MHz.			

4.5.8.3 Conformance

The conformance tests for this requirement shall be as described in clause 5.3.8.

4.5.9 Internal immunity

4.5.9.1 Definition

Internal immunity is the level of the unwanted cross modulation product relative to the wanted signal at the output of an amplifier or active antenna when a three tone test signal is applied at the input. The 3 tone test signal comprises a wanted carrier and two unwanted carriers at a given set of test frequencies.

4.5.9.2 Limits

The amplifier internal immunity limits shall not exceed the class-dependent values given in Tables 16.1 and 16.2 at the defined test frequencies.

Table 16.1: Category

{P,D,L}{1}internal immunity limits

Unwanted Signals			Wanted Signal		Internal immunity (dBc)
$F_{u,1}$ (MHz)	$F_{u,2}$ (MHz)	$P_{u\{1,2\}}$ (dBm)	$F_{w.}$ (MHz)	P_w (dBm)	
398	399	-25	470	-25	-35
			586		
			686		
703	704	-15	470	-25	-35
			586		
			686		
738	739	0	470	-25	-35
			586		
			686		
174	175	-25	205,5	-25	-35
229	230	-25	205,5	-25	-35

Table 16.2: Category

{P,D,L}{2} internal immunity limits

Unwanted Signals			Wanted Signal		Internal immunity (dBc)
$F_{u,1}$ (MHz)	$F_{u,2}$ (MHz)	$P_{u\{1,2\}}$ (dBm)	$F_{w.}$ (MHz)	P_w (dBm)	
398	399	-25	478	-25	-35
			586		
			686		
466	467	-15	478	-25	-35
			586		
			686		
703	704	-15	478	-25	-35
			586		
			686		
738	739	0	478	-25	-35
			586		
			686		
174	175	-25	205,5	-25	-35
229	230	-25	205,5	-25	-35

The active antenna internal immunity limits shall not exceed the class-dependent limit values given in Tables 17.1 and 17.2 at the defined test frequencies.

Table 17.1: Category

{A}{1}internal immunity limits

Unwanted Signals			Wanted Signal		Internal immunity (dBc)
$F_{u,1}$ (MHz)	$F_{u,2}$ (MHz)	$E_{u\{,1,2\}}$ (dBμV/m)	$F_{w.}$ (MHz)	E_w (dBμV/m)	
398	399	109	470	109	-35
			586		
			686		
703	704	119	470	109	-35
			586		
			686		
738	739	124	470	109	-35
			586		
			686		
174	175	109	205,5	109	-35
229	230	109	205,5	109	-35

Table 17.2: Category

{A}{2}internal immunity limits

Unwanted Signals			Wanted Signal		Internal immunity (dBc)
$F_{u,1}$ (MHz)	$F_{u,2}$ (MHz)	$P_{u\{1,2\}}$ (dBμV/m)	$F_{w.}$ (MHz)	P_w (dBμV/m)	
398	399	109	478	109	-35
			586		
			686		
466	467	119	478	119	-35
			586		
			686		
703	704	119	478	109	-35
			586		
			686		
738	739	124	478	109	-35
			586		
			686		
174	175	109	205,5	109	-35
229	230	109	205,5	109	-35

4.5.9.3 Conformance

The conformance tests for this requirement shall be as described in clause 5.3.9.

5 Testing for compliance with technical requirements

5.1 Environmental conditions for testing

Tests defined in the present document shall be carried out at representative points within the boundary limits of the declared operational environmental profile.

Where technical performance varies subject to environmental conditions, tests shall be carried out under a sufficient variety of environmental conditions (within the boundary limits of the declared operational environmental profile) to give confidence of compliance for the affected technical requirements.

5.2 Void

5.3 Methods of measurement

5.3.1 Void

Figure 5: Void

5.3.2 Noise figure

The noise figure shall be measured with a calibrated noise generator operating in the frequency band of use for the AUT together with a spectrum analyser.

NOTE 1: An automatic noise figure instrument, if available, may provide an automation of the process described and replaces the spectrum analyser in the test method.

The measurement method is known as the "Y-Factor Method" and uses a noise generator with a calibrated Excess Noise Ratio (ENR). The ENR is defined as:

$$ENR_{dB} = 10 \times log_{10}[\frac{T_s^{On} - T_s^{Off}}{T_0}]$$

where: T_s^{On} is the noise temperature of the noise source in its "on state";

T_s^{Off} is the noise temperature of the noise source in its "off state"; and

T_0 is the reference noise temperature (290 K).

The AUT shall be connected as shown in Figure 6. The cable connection between the noise generator and the AUT should be kept as short as possible. The impedances of all test equipment shall be adapted to that of the AUT.

NOTE 2: Impedance transformers are preferable to matching attenuators to maintain the noise floor of the spectrum analyser.

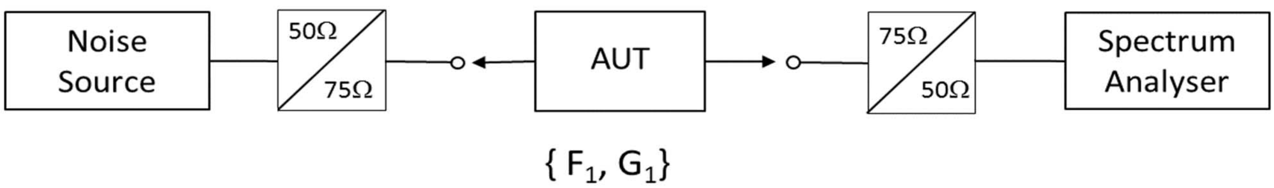


Figure 6: Measurement arrangements for noise figure test

The following measurement procedure shall be followed:

1) Set the spectrum analyser to a reference level appropriate for the AUT. Set the analyser to zero span, at the required test frequency. Set the detector to "rms" (for analysers that do not have an rms detector, the sample detector is recommended as an alternative), the sweep time to 20 seconds, the number measurement points to 501 (the number of measurement points cannot be altered on some analysers; alternatives to 501 may also be satisfactory dependent upon the analyser characteristics), the video bandwidth to 300 kHz (the video bandwidth setting is disabled on some analysers when the rms detector is selected), and the resolution bandwidth to 100 kHz to give a smooth trace with noise ripples < 0,25 dB. Set the spectrum analyser input attenuator to 0 dB and enable its pre-amplifier (where fitted).

2) Disconnect the AUT and terminate the input to the spectrum analyser with a 75 Ω load and record the displayed average noise level, p_{DANL}.

Reconnect the AUT and record the level in dBm of the amplified noise with the noise source in its off state, p_{off}. Calculate the noise corrected value, $p_{off,corr}$, using:

$$p_{off,corr} = 10 \times log_{10}(10^{\left(\frac{p_{off}}{10}\right)} - 10^{\left(\frac{p_{DANL}}{10}\right)})$$

3) Record the level of the amplified noise with the noise source in its on state, p_{on}. Calculate the noise corrected value, $p_{on,corr}$, using:

$$p_{on,corr} = 10 \times log_{10}(10^{\left(\frac{p_{on}}{10}\right)} - 10^{\left(\frac{p_{DANL}}{10}\right)})$$

4) Calculate the Y factor:

$$Y = 10^{((p_{on,corr} - p_{off,corr})/10)}$$

5) Calculate and record the value of the noise figure for the AUT thus:

$$nf = ENR_{dB} - 10 \times log_{10}(Y - 1)$$

Repeat step 1) to step 5) at the specified test frequencies.

5.3.3 Amplifier intermodulation

Two equal amplitude, sinusoidal, non-harmonically related tones at 100 kHz above and below the required test frequency shall be injected by means of a combiner to the AUT input. The linearity of the signal generators and the combining arrangement shall be checked on a spectrum analyser and adjustments made to ensure that any third order intermodulation products (see clause 4.5.3.1) in the generators are below -55 dBc.

The third order products shall be measured with a spectrum analyser as shown in Figures 7 and 8.

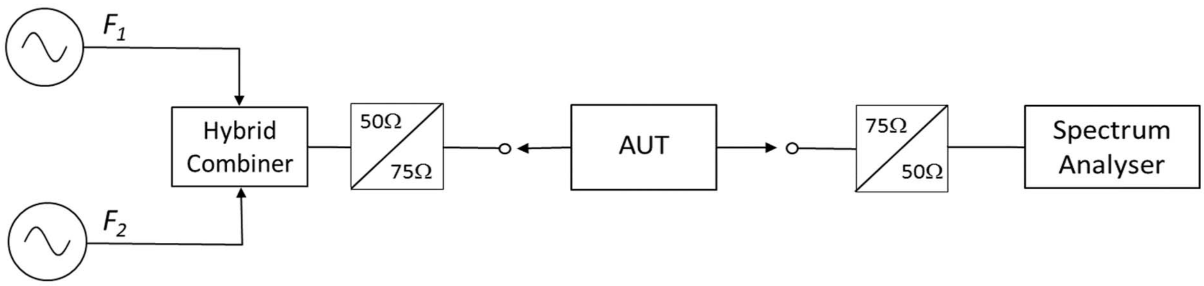


Figure 7: Measurement arrangement for intermodulation test

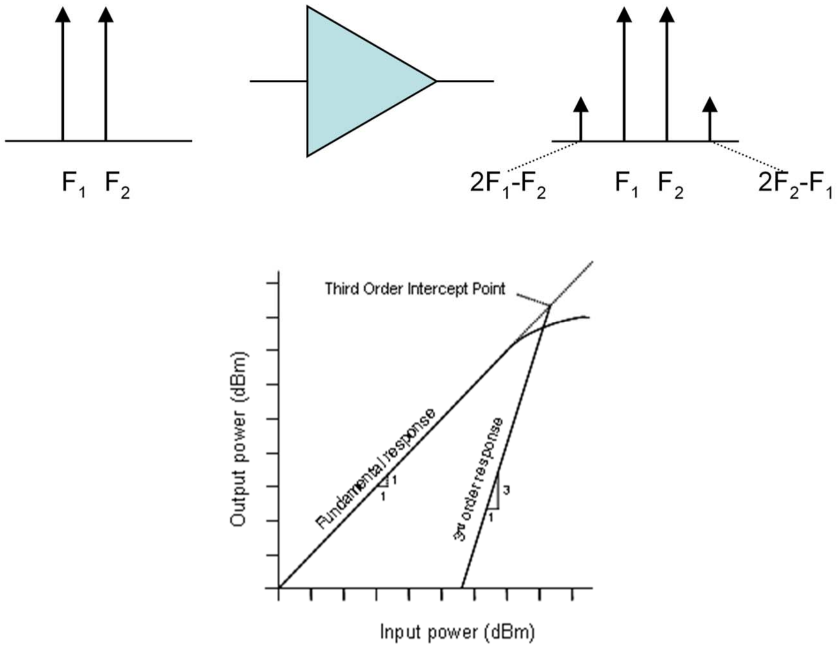


Figure 8: Third order IMD illustration

The level of each of the two tones shall be increased to a level p_{in}, until the larger of the two third order (IM3) products is between 38 dB and 42 dB below that of the wanted two tones at the output. The relative level of the worst product (IM3) shall be recorded.

The input referred, Third Order Intercept (TOI) expressed in the log domain is given by:

$$TOI_{input} = p_{in} + \frac{IM3}{2}$$

where:

p_{in} is the level of each tone at the amplifier input expressed in dBm;

IM3 is the measured relative level of the worst third order intermodulation product, i.e. between 38 dBc and 42 dBc.

For variable gain amplifiers, the gain shall be set to maximum. For amplifiers fitted with slope controls, the slope shall be set to the flat position.

The test shall be repeated at the specified test frequencies.

5.3.4 Return loss

Return loss shall be measured with a network analyser, which shall be calibrated. The network analyser source power shall be chosen to prevent saturation of the AUT. Precision RF adaptors and cable assemblies, designed for constant impedance, shall be used to minimize degradation of the measured return loss.

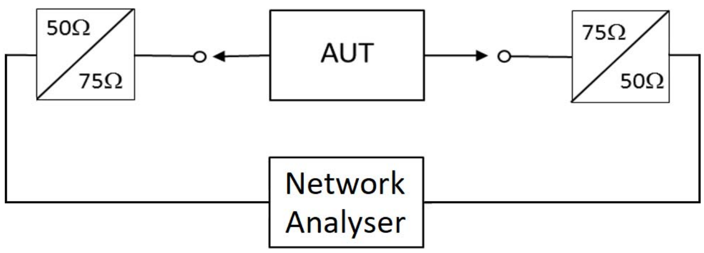


Figure 9: Return loss measurement arrangements

5.3.5 Selectivity

The selectivity measurement shall be made with a spectrum analyser equipped with an RF tracking generator as shown in Figure 10. The output level of the tracking generator shall be set at an appropriate power level and connected to the input port of the AUT. The gain shall be measured across the specified frequency range.

If the amplifier gain can be varied, the test shall be carried out at the maximum gain. For amplifiers fitted with slope controls, the slope shall be set to the flat position.

Figure 10: Amplifier frequency response measurement test arrangement

The amplifier gain in the log domain, $g(dB)$, is defined by:

$$g(f) = 10 \times log_{10}(P_{out}/P_{in})$$

where:

P_{out} is the output power; and

P_{in} is the input power measured in the linear domain (W).

The gain variation is defined as the difference between the maximum and minimum gain measured over the specified test frequencies.

5.3.6 Active antenna gain

This shall be measured using a GTEM cell as shown in Figure 11.

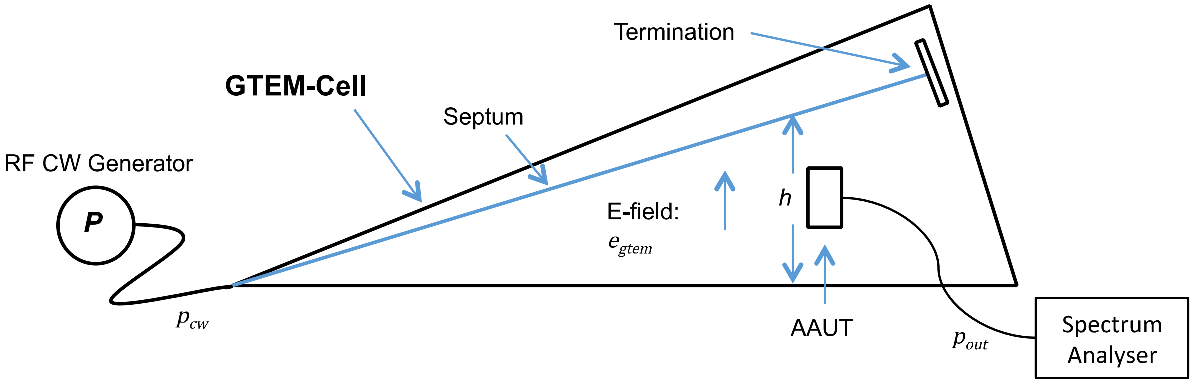


Figure 11: Active antenna gain test arrangement

The Active Antenna Under Test (AAUT) should be positioned at the optimum location within the GTEM cell, as specified by the cell manufacturer, taking into account the polarization of the generated field and the directivity of the AAUT. For variable gain AAUTs the gain shall be set to maximum.

Connections between the AAUT and the outside world shall be arranged to avoid common-mode effects and the ingress of interference. Common mode effects can be reduced by placing the AAUT on the floor of the GTEM cell, but the calibration of the GTEM cell will need to be adjusted to account for this.

The electric field, e_{gtem}, expressed in dBµV/m seen by the AAUT shall be derived from the input power to the GTEM cell, p_{cw}, expressed in dBm using the relevant calibration data (see annex B). The gain of the AAUT is given by:

$$g_{aaut} = (g_i + g_a) = 77{,}2 + 20 \times log_{10}(f_{MHz}) + p_{out,cw} - e_{gtem,cw}$$

where:

$p_{out,cw}$ is the output power in dBm at the output port of the AAUT;

$e_{gtem,cw}$ is the electric field in dBµV/m seen by the AAUT within the GTEM cell.

An electric field, $e_{gtem,cw}$ = 70 dBµV/m shall be used for the tests.

5.3.7 Active antenna figure of merit

The antenna gain, g_{aaut}, at the specified test frequencies shall first be measured using the method described in clause 5.3.6.

With the AAUT in a GTEM cell with no RF signal applied, the noise power, p_n , delivered to the spectrum analyser by the AAUT shall be measured in an 8 MHz bandwidth with a spectrum analyser using the channel power measurement function.

The figure of merit (FoM) for the AAUT shall be calculated using:

$$FoM = (g_i - f_a) = -105 - p_n + g_{aaut}$$

The measurements shall be repeated at the specified test frequencies.

5.3.8 Active antenna intermodulation

The active antenna should be positioned in the GTEM cell as shown in Figure 12.

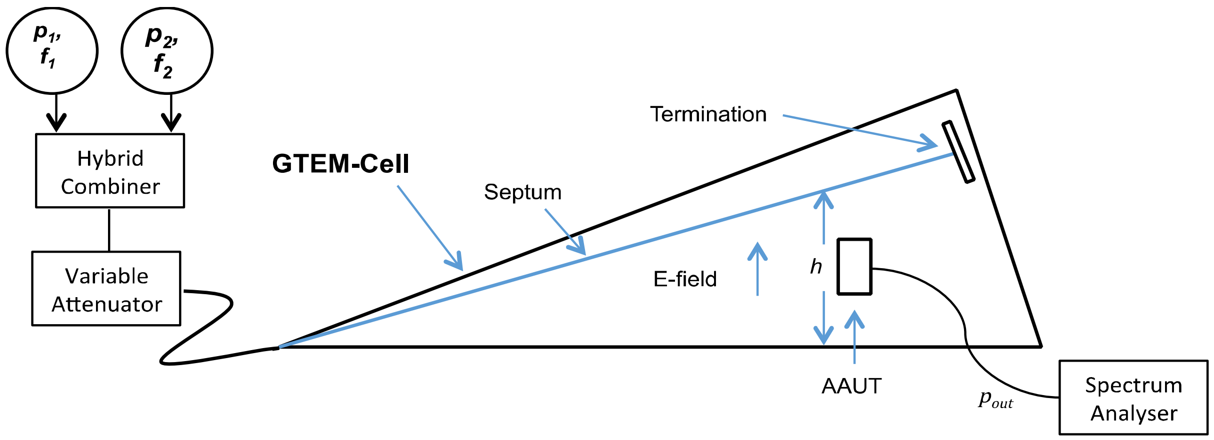


Figure 12: Active antenna intermodulation test arrangement

Two equal amplitude, sinusoidal, non-harmonically related tones at ±100 kHz from the required test frequency shall be injected by means of a combiner to the AAUT as shown in Figure 12. Note the linearity of the signal generators and the combining arrangement should be checked on a spectrum analyser to ensure any third order intermodulation products from the generators are below -55 dBc.

The third order products on the output signal, p_{out}, are measured, with a spectrum analyser.

The level of each of two tones shall be increased using the variable attenuator until the larger of the two third order (IM3) products measured on the spectrum analyser is between 38 dB and 42 dB below the wanted two tones at the output.

The input referred, Third Order Intercept (TOI) expressed in the log domain is given by:

$$e_{toi} = p_{out} + \frac{IM3}{2} + (77{,}2 + 20 \times log_{10}(f_{MHz}) - g_{aaut})$$

where:

- p_{out} is the level of each of the tone at the amplifier input expressed in dBm;
- $IM3$ is the measured level of the worst third order intermodulation product, i.e. between 38 dBc and 42 dBc;
- f_{MHz} is the centre frequency of the two tones in MHz used for the test;
- g_{aaut} is the active antenna gain measured using the procedure in clause 5.3.6.

The measurement shall be repeated for each of the specified test frequencies.

The calibration of the GTEM cell is not important for this measurement as the calibrated gain measurement, g_{aaut}, is used to calculate the input intercept from the measured output intercept ($p_{out} + \frac{IM3}{2}$). It is sometimes useful to place the AAUT above the septum of the GTEM cell to reduce the level of the signal required from the signal generators.

5.3.9 Internal immunity

5.3.9.1 Method of measurement for active antennas

The AAUT should be positioned in the GTEM cell as shown in Figure 13. The test signals shall be applied to the chamber to generate the fields specified in Table 17.1 or Table 17.2, taking account of the calibration of the GTEM cell. The spectrum analyser is tuned to the frequency of the wanted signal. Immunity, I, is the difference in power, expressed in decibels, between the wanted signal and the higher of the two sidetones at ±1 MHz relative to the wanted signal. For each test configuration, the AAUT immunity should not exceed the limit values given in Table 17.1 or Table 17.2.

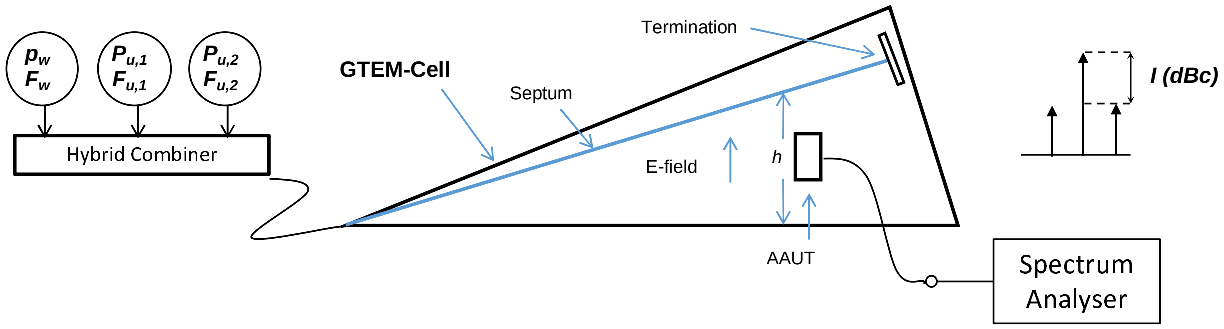


Figure 13: Active antenna immunity test arrangement

Note the linearity of the signal generators and the combining arrangement should be checked on a spectrum analyser to ensure any third order intermodulation products from the generators are below -35 dBc with respect to $P_{u,1}$ and $P_{u,2}$. Third order products from the generator arrangement should be checked at ($2 \times F_{u,1} - F_{u,2}$) and ($2 \times F_{u,2} - F_{u,1}$). It is sometimes useful to place the AAUT above the septum of the GTEM cell to reduce the level of the signal required from the signal generators.

5.3.9.2 Method of measurement for amplifiers

The AUT should be connected to the test sources as shown in Figure 14. The test signal levels shall be applied to the AUT as detailed in Table 16.1 or Table 16.2, taking into account cable losses and the combiner losses. The spectrum analyser is tuned to the frequency of the wanted signal. Immunity, I, is the difference in power, expressed in decibels, between the wanted signal and the higher of the two sidetones at ±1 MHz relative to the wanted signal. For each test configuration, the AUT immunity should not exceed the limit values given in Table 16.1 or Table 16.2.

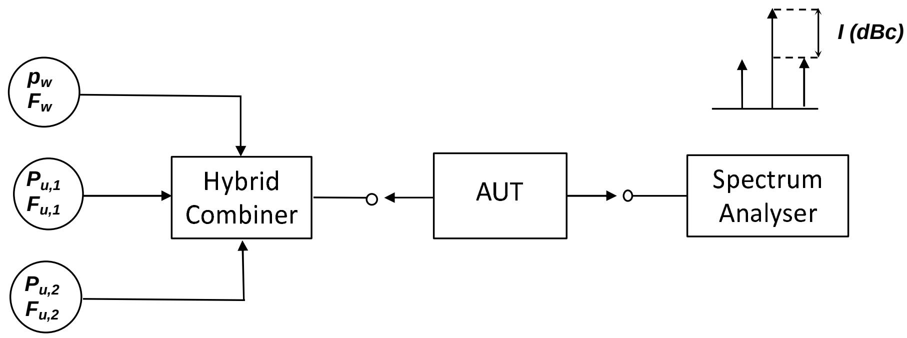


Figure 14: Amplifier immunity test arrangement

Note the linearity of the signal generators and the combining arrangement should be checked on a spectrum analyser to ensure any third order intermodulation products from the generators are below -35 dBc with respect to $P_{u,1}$ and $P_{u,2}$. Third order products from the generator arrangement should be checked at $(2 \times F_{u,1} - F_{u,2})$ and $(2 \times F_{u,2} - F_{u,1})$.

Annex A (informative): Relationship between the present document and the essential requirements of Directive 2014/53/EU

The present document has been prepared under the Commission's standardisation request C(2015) 5376 final [i.4] to provide one voluntary means of conforming to the essential requirements of Directive 2014/53/EU on the harmonisation of the laws of the Member States relating to the making available on the market of radio equipment and repealing Directive 1999/5/EC [i.1].

Once the present document is cited in the Official Journal of the European Union under that Directive, compliance with the normative clauses of the present document given in Table A.1 confers, within the limits of the scope of the present document, a presumption of conformity with the corresponding essential requirements of that Directive, and associated EFTA regulations.

Table A.1: Relationship between the present document and the essential requirements of Directive 2014/53/EU

Harmonised Standard ETSI EN 303 354					
Requirement				Requirement Conditionality	
No	Description	Essential requirements of Directive 2014/53/EU	Clause(s) of the present document	U/C	Condition
1	Noise figure	3.2	4.5.2	C	Equipment category {P, D ,L}
2	Amplifier intermodulation	3.2	4.5.3	C	Equipment category {P, D ,L}
3	Return loss	3.2	4.5.4	C	Equipment category {P, D ,L}
4	Selectivity	3.2	4.5.5	U	
5	Active antenna gain	3.2	4.5.6	C	Equipment category {A}
6	Active antenna figure of merit	3.2	4.5.7	C	Equipment category {A}
7	Active antenna intermodulation	3.2	4.5.8	C	Equipment category {A}
8	Internal immunity	3.2	4.5.9	U	

Key to columns:

Requirement:

No A unique identifier for one row of the table which may be used to identify a requirement.

Description A textual reference to the requirement.

Essential requirements of Directive

Identification of article(s) defining the requirement in the Directive.

Clause(s) of the present document

Identification of clause(s) defining the requirement in the present document unless another document is referenced explicitly.

Requirement Conditionality:

U/C Indicates whether the requirement is unconditionally applicable (U) or is conditional upon the manufacturer's claimed functionality of the equipment (C).

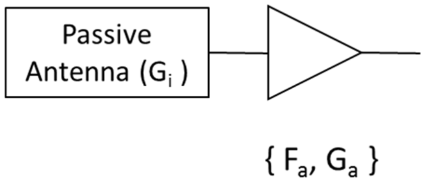
Condition Explains the conditions when the requirement is or is not applicable for a requirement which is classified "conditional".

Presumption of conformity stays valid only as long as a reference to the present document is maintained in the list published in the Official Journal of the European Union. Users of the present document should consult frequently the latest list published in the Official Journal of the European Union.

Other Union legislation may be applicable to the product(s) falling within the scope of the present document.

Annex B (informative): Active Antenna Theory

Consider an active antenna comprising a passive antenna with gain G_i relative to an isotropic radiator connected to an amplifier with a noise factor F_a and a gain G_a (all quantities in the linear domain).



The antenna aperture, A_e , is given by:

$$A_e = G_i \times \frac{\lambda^2}{4\pi}$$

And the power, P, delivered by the active antenna illuminated by an electric field E (V/m) is given by:

$$P = \frac{E^2}{Z_0} \times A_e \times G_a = \frac{E^2}{377} \times \frac{\lambda^2}{4\pi} \times G_i \times G_a = \frac{E^2 \lambda^2}{1\,508 \times \pi} \times G_i \times G_a = \frac{E^2 c^2}{1\,508 \times \pi \times f^2} \times G_i \times G_a$$

where:

- Z_0 is the impedance of free space (nominally 377 Ω);
- E is the incident electric field (V/m);
- λ is the wavelength of the incident electric field (m);
- c is the speed of light in free space (2,998 × 10^8 m/s);
- f is the frequency (Hz).

Note all quantities are measured in the linear domain. Converting to the log (dB) domain:

$$p_{dBW} = 10 \times log_{10}\left(\frac{c^2}{1\,508 \times \pi}\right) + 20 \times log_{10}(E) - 20 \times log_{10}(f) + 10 \times log_{10}(G_i) + 10 \times log_{10}(G_a)$$

$$p_{dBW} = 10 \times log_{10}\left(\frac{c^2}{1\,508 \times \pi}\right) + e_{\frac{dBV}{m}} - 20 \times log_{10}(f) + g_i + g_a$$

where:

- p_{dBW} is the power delivered by the antenna in dB relative to 1 W;
- $e_{dBV/m}$ is the incident electric field in dB relative to (1 V/m);
- g_i is the antenna gain in the log domain relative to an isotropic antenna (dBi);
- g_a is the amplifier gain in the log domain (dB).

Scaling to power relative to 1 mW, p_{dBm}, at a frequency, f_{MHz}, for an electric field, $e_{dB\mu V/m}$ gives:

$$p_{dBm} = -30 + 10 \times log_{10}\left(\frac{c^2}{1\,508 \times \pi}\right) + (e_{\frac{dB\mu V}{m}} - 120) - (120 + 20 \times log_{10}(f_{MHz})) + g_i + g_a$$

$$p_{dBm} = \left\{10 \times log_{10}\left(\frac{c^2}{1\,508 \times \pi}\right) - 210\right\} + e_{dB\mu V/m} - 20 \times log_{10}(f_{MHz}) + g_i + g_a$$

$$p_{dBm} = -77{,}2 + e_{dB\mu V/m} - 20 \times log_{10}(f_{MHz}) + g_i + g_a$$

The active antenna gain, g_{aaut}, can thus be calculated from the output power , p_{dBm}, from an AAUT illuminated by a known electric field , $e_{dB\mu V/m}$, using:

$$g_{aaaut} = g_i + g_a = p_{dBm} + 77{,}2 - e_{dB\mu V/m} + 20 \times log_{10}(f_{MHz})$$

A useful Figure of Merit (FoM) for an active antenna is the passive antenna gain, g_i, less the amplifier noise figuref_a. Increasing the passive gain, g_i, or decreasing the noise figure, f_a, will improve reception in a typical application.

The power, P_N, in mW, delivered by an active antenna in a GTEM cell with no E field applied measured in a bandwidth of B_{MHz} is given by:

$$P_N = 1\,000 \times G_a F_a k T B_{MHz}$$

Converting to the log domain (dB), the power referenced to 1 mw, $p_{n,dbm}$, is given by:

$$p_{n,dBm} = g_a + f_a + 10 \times log_{10}(kT) + 10 \times log_{10}(B_{MHz}) + 30$$

$$p_{n,dBm} = g_a + f_a + 10 \times log_{10}(B_{MHz}) - 114$$

Substituting:

$$g_a = g_{aaut} - g_i$$

Gives:

$$p_{n,dBm} = g_{aaut} - g_i + f_a + 10 \times log_{10}(B_{MHz}) - 114$$

Rearranging this equation allows the antenna Figure of erit, FoM, to be calculated from the active antenna gain and the noise power delivered by an unilluminated antenna:

$$FoM = (g_i - f_a) = -114 + 10 \times log_{10}(B_{MHz}) - p_{n,dBm} + g_{aaut}$$

Annex C (informative): Maximum measurement uncertainty

The measurements described in the present document are based on the following assumptions:

- the measured value related to the corresponding limit is used to decide whether an equipment meets the requirements of the present document;
- the value of the measurement of each parameter is included in the test report.

For the test methods, the recommended values of the measurement uncertainty are calculated and correspond to an expansion factor (coverage factor) k = 1,96 (which provide confidence levels of 95 % in the case where the distributions characterizing the actual measurement uncertainties are normal (Gaussian)). Principles for the calculation of measurement uncertainty are contained in ETSI TR 100 028 [i.6].

Table C.1 shows the recommended values for the maximum measurement uncertainty figures.

Table C.1: Maximum measurement uncertainty

Parameter	Uncertainty
Radio frequency	$\pm 1 \times 10^{-7}$
Radiated RF power	±6 dB
Conducted RF power variations using a test fixture	±0,75 dB

Annex D (informative): Change history

Version	Information about changes
V1.1.1	First published version.
V1.2.1	Revised to take account of changes to the upper frequency of the UHF broadcast band: classes 0, 3, 4 are removed as no longer applicable.

History

Document history		
V1.1.1	March 2017	Publication
V1.1.8	June 2024	SRdAP process EV 20240925: 2024-06-27 to 2024-09-25